

# Centrifugal pump simulation during waterhammer analysis

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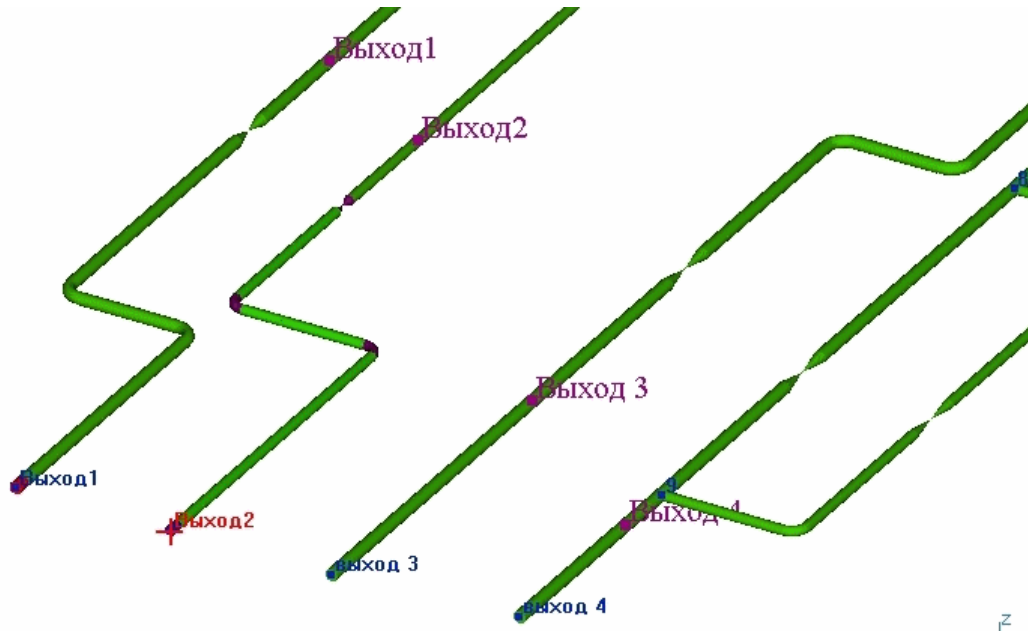
November 30 - December 4

**AT THE  
EPICENTRE  
OF THE  
DIGITAL  
TRANSFORMATION  
OF INDUSTRY**

**36<sup>th</sup> INTERNATIONAL CAE  
CONFERENCE AND EXHIBITION**

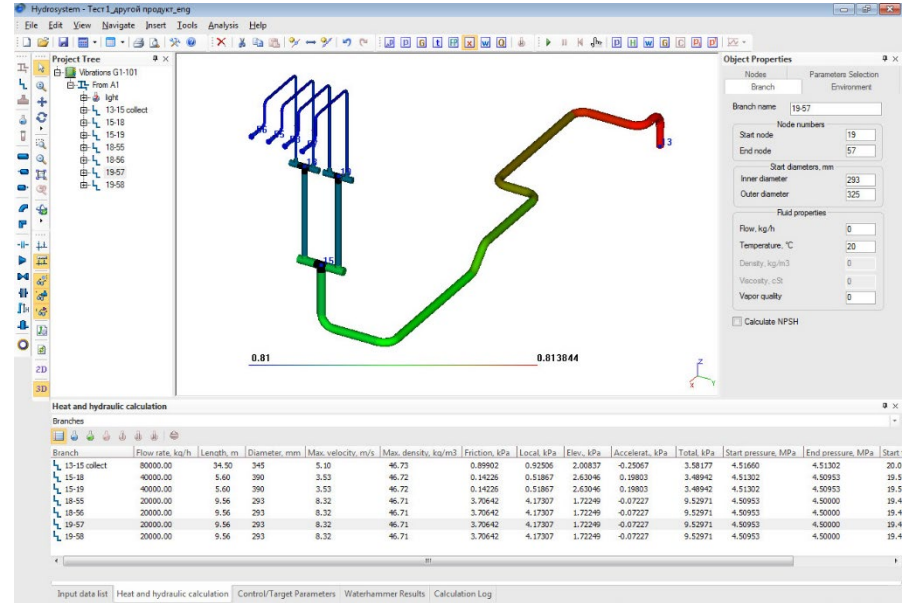
# Where we have met dynamic pump simulation?

- PASS/HYDROSYSTEM software
  - Surge add-on module



# PASS/Hydrosystem | Experience and popularity

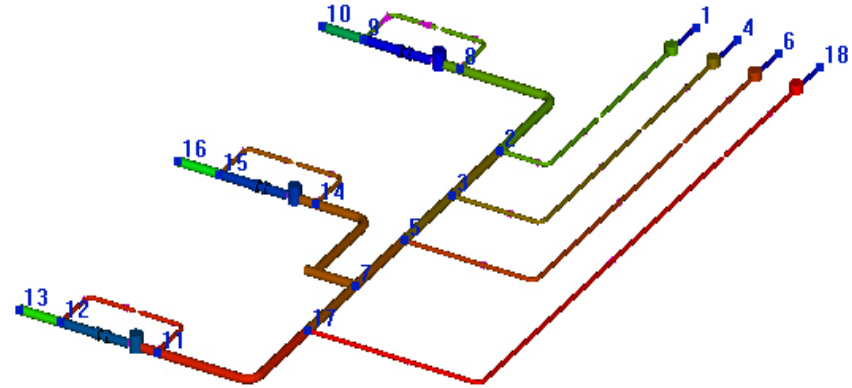
- Part of PASS product family
- First introduced in 1977
- Blessed by piping hydraulic world-known “guru” Idelchik
- Used by more than 600 companies worldwide
- Ideal tool for “day-to-day” operations in designing of any piping systems



PIPING AND EQUIPMENT  
ANALYSIS & SIZING SUITE

# PASS/Hydrosystem | Calculation capabilities

- Heat and hydraulic calculation of steady-state flow for:
  - Liquids
  - Real gases
  - Gas-liquid mixtures
  - Gas-liquid-liquid mixtures
  - Liquid-solid mixtures (a.k.a. 'slurry' flow)
- Surge analysis of transient liquid flow – water-hammer calculation
- Unbalanced forces calculation and transfer to PASS/START-PROF and other piping stress analysis software
- Suitable for piping systems of any complexity



PIPING AND EQUIPMENT  
ANALYSIS & SIZING SUITE

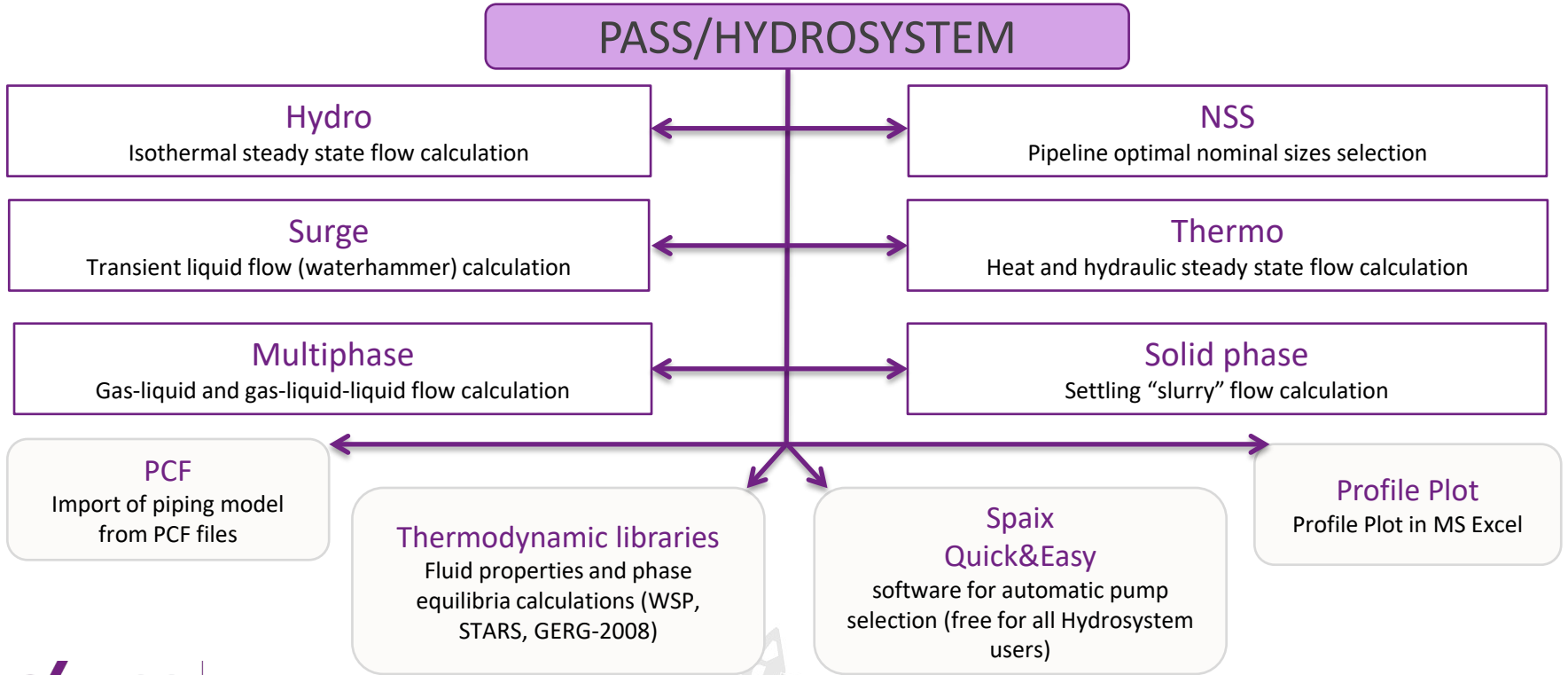
t

89.99

180.07 °C

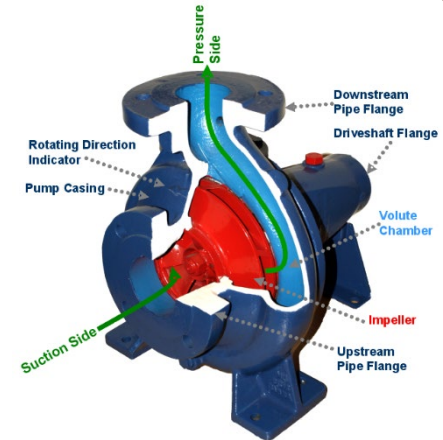
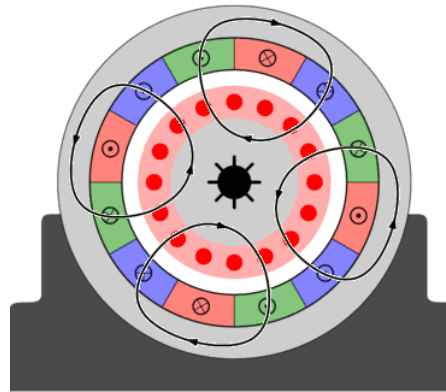
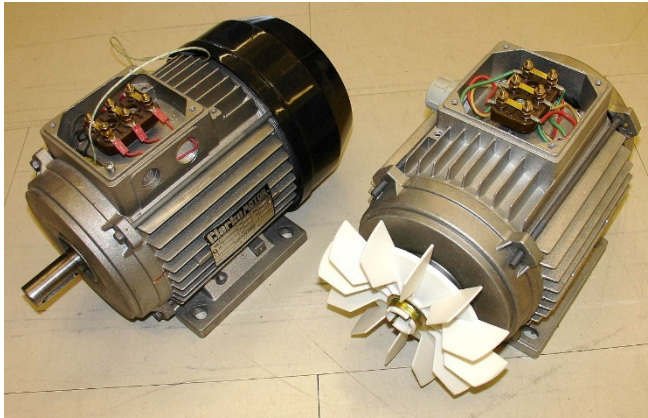
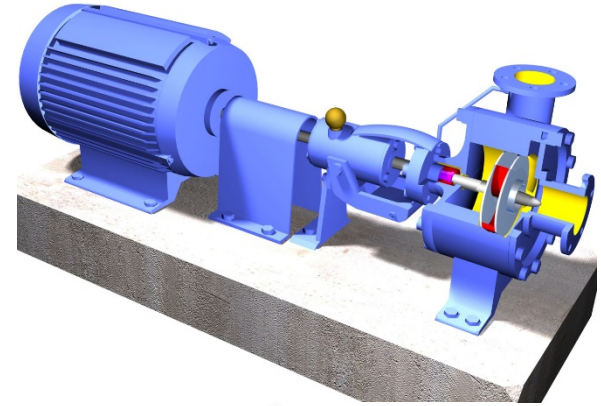


# PASS/Hydrosystem | Modules and features



# What type of pumps we are talking about?

- Centrifugal (or more general, rotodynamic) pump
- + Induction (or asynchronous) motor



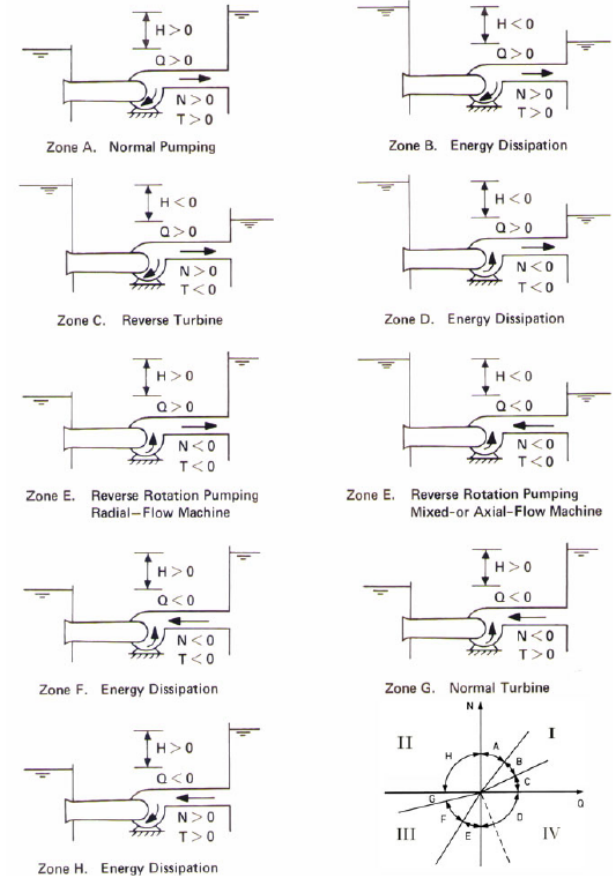
# What transient operations we need to simulate?

- Pump start-up (pump switched off -> operating at duty point)
  - From stopped pump (discharge valve closed) or from flow through non-operating pump
- Pump shut down (operating at duty point - >switched off)
- Pump is operating, transient from one duty point to another (pump is switched on, event is in piping system)
- Transient in non-operating opened pump (pump is switched off, event is in piping system)



# Transient vs steady state modeling for pumps

- Curves from Manufacturer for steady-state operation
  - $H(Q)$ ,  $P(Q)$  or Efficiency( $Q$ ),  $NPSH_r(Q)$  for some nominal  $n$  (speed of rotation)
  - Limited zone of operation parameters
- In transient mode pump can go through unusual regimes (4 quadrants) with arbitrary  $Q$  and  $n$  !





# Mathematical model of the pump

- Equation of Torque balance
  - $2\pi J \frac{dn}{dt} = T_{motor}(n) - T_{pump}(Q, n)$
  - $J = J_{rotor} + J_{impeller} + J_{fluid}$
- Boundary conditions on pump for inlet and discharge piping (analysis by characteristic method)
  - $H_{outlet} - H_{inlet} = H(Q, n)$
- How to calculate  $T_{motor}(n)$ ,  $T_{pump}(Q, n)$ ,  $H(Q, n)$

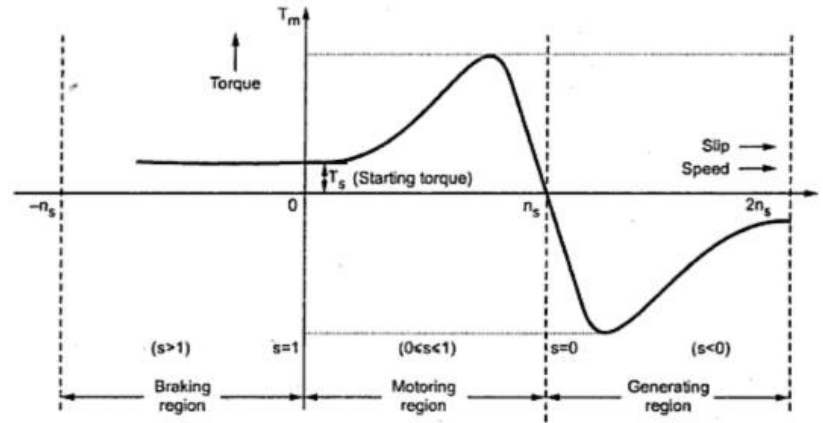
# Mathematical model of asynchronous motor

- Slip  $s = \frac{n_s - n}{n_s}$

- $T_{motor}(n) = \frac{2T_{cr}}{\frac{s}{s_{cr}} + \frac{s_{cr}}{s}}$

- For specific motor manufacturer usually gives

- Stator magnetic field rotation  $n_s = \frac{2f}{p}$ ,  
 $f$  – frequency of power supply,  $p$  – number of magnetic poles
- $T_{cr}, n_{cr}$  (critical parameters)
- $T_{nom}, n_{nom}$  (nominal parameters)
- $J_{rotor}$



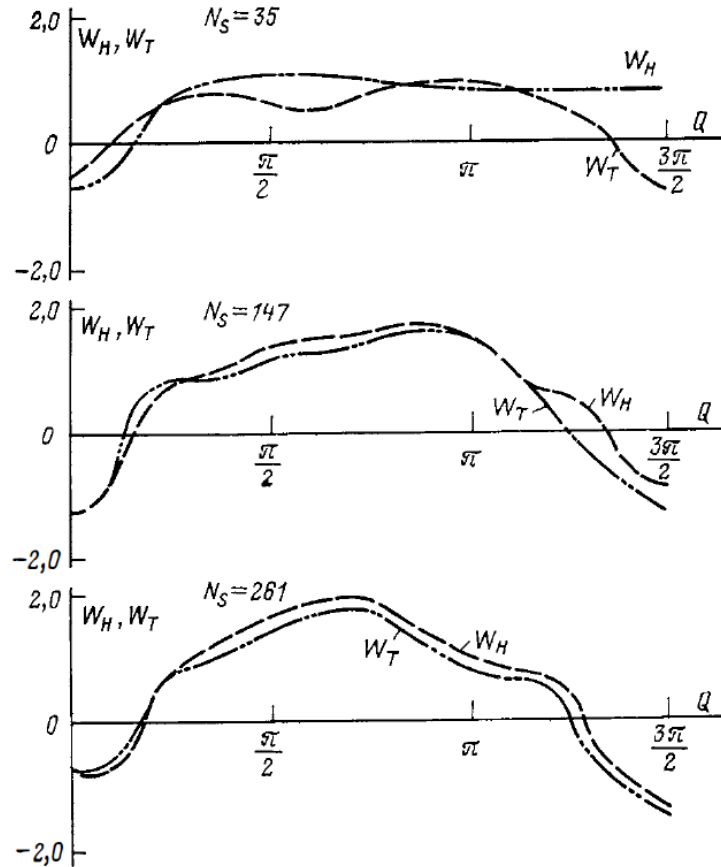
# General description of pump by Suter curves

- To calculate  $T_{pump}(Q, n)$ ,  $H(Q, n)$  for turbulent quadratic flow, let's use affinity laws:  $H$  and  $T \sim Q^2$  and  $n^2$
- Defining dimensionless Suter curves as
  - $\theta = \tan^{-1}\left(\frac{n}{n_{nom}} \frac{Q_{nom}}{Q}\right)$
  - $W_H(\theta) = \text{sign}(H) \sqrt{\frac{|H|/H_{nom}}{(Q/Q_{nom})^2 + (n/n_{nom})^2}}$
  - $W_T(\theta) = \text{sign}(T) \sqrt{\frac{|T|/T_{nom}}{(Q/Q_{nom})^2 + (n/n_{nom})^2}}$
  - Where  $Q_{nom}$ ,  $n_{nom}$ ,  $H_{nom}$ ,  $T_{nom}$  - values in pump B.E.P.

# Where to find Suter curves?

- Using Suter curves we can calculate  $T_{pump}(Q, n)$ ,  $H(Q, n)$
- But pump manufacturers don't want to provide them...
- But there is some data for specific pumps!
- So we can try to use Suter curves for similar pump (or interpolate between several)
- How to define if pump is “similar”? Usually by the value of “Specific speed”: 
$$N_s = \frac{n_{nom} Q_{nom}}{H_{nom}^{0.75}}$$

# Suter curves on Donsky's data



# How to merge Suter curves with usual pump curve?

- For pump transient simulation we use Suter curves
- For pump steady state simulation we use “traditional” pump curves from manufacturer
- But they have to coincide with each other in corresponding region of  $\theta$  values, otherwise simulation can give non-adequate results!
- We should correct general  $W_H(\theta)$  for specific pump using  $H(Q)$  curve from pump manufacturer!
- But... there is one important aspect to take into account!

# “Floating” $n$ and how to count it

- $n$  is not equal to  $n_{nom}$  all over the manufacture  $H(Q)$  curve
  - It is slightly “floating” between  $n_{cr}$  and  $n_s$ !
  - Do manufactures really recalculate  $H(Q)$  to  $n_{nom}$  to take this into account? Most likely no – we always use  $H(Q)$  in steady state analysis without any correction
  - How to count it?
- Get real value of  $n$  (for fixed value of  $Q$  or  $\theta$ ) from equation
  - $T_{motor}(n) = W_T^2(\theta)[(Q/Q_{nom})^2 + (n/n_{nom})^2]T_{nom}$
- Then get corrected value of  $W_H(\theta)$  using this value of  $n$



# Dimensionless Torque Equation

- Equation

- $2\pi J \frac{dn}{dt} = T_{motor}(n) - T_{pump}(Q, n)$

- Can be put in dimensionless form

- $T_r \frac{d\beta}{dt} = \frac{1}{T_{nom}} [T_{motor}(\beta) - T_{pump}(q, \beta)]$

- $\beta = n/n_{nom}, q = Q/Q_{nom}$

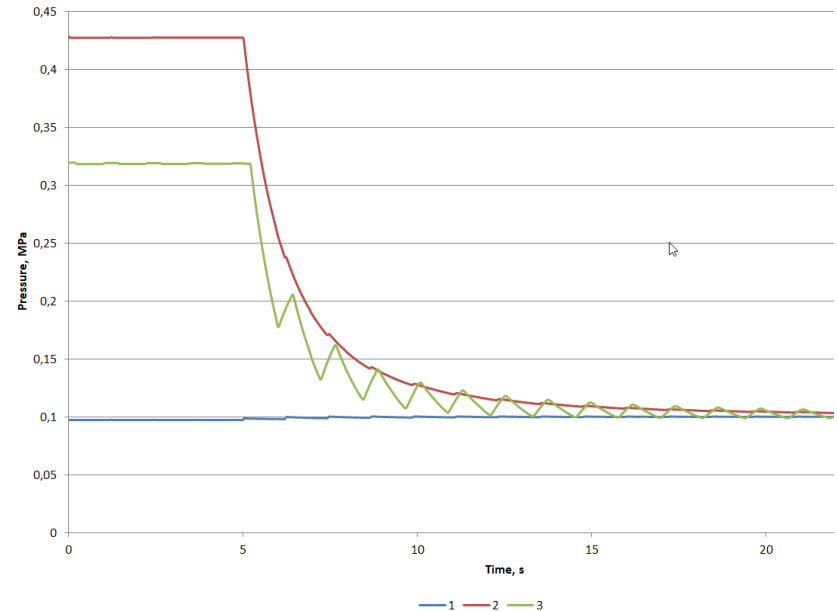
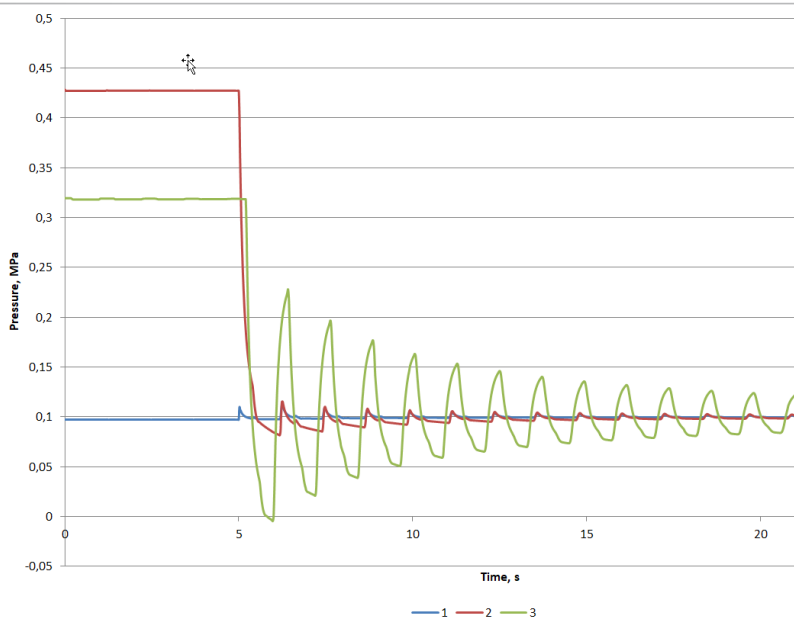
- $T_r = 2\pi J n_{nom} / T_{nom} > 2\pi J_{motor} n_{nom} / T_{nom}$  is time characterizing pump transient behavior (usually from 0.05 to 5 s)

# Pump start-up and shut down – rule of thumb

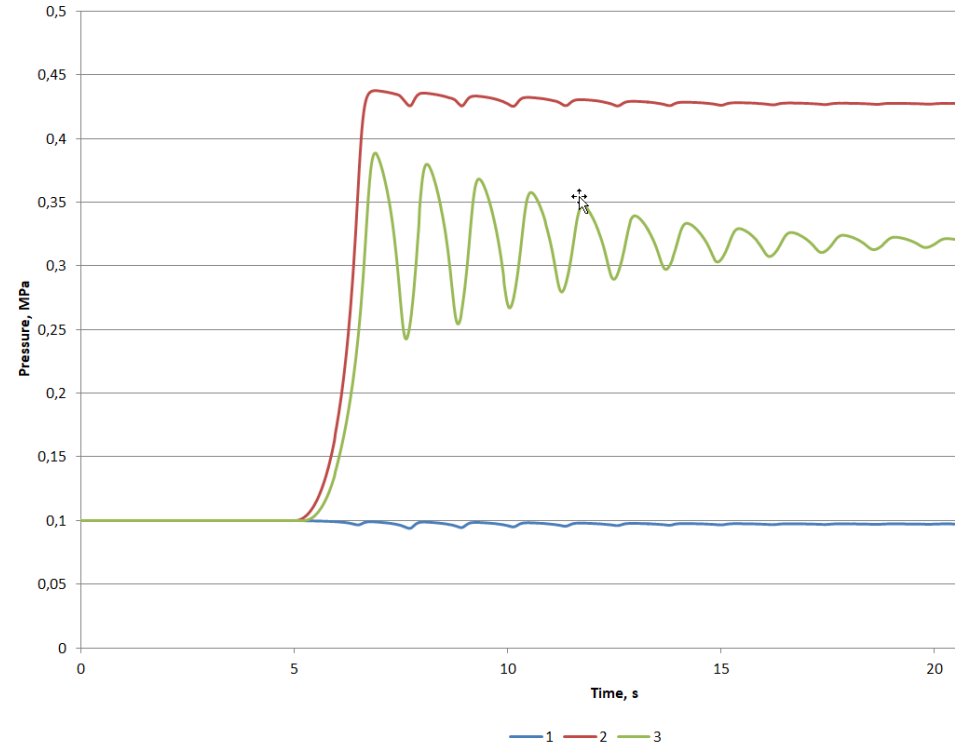
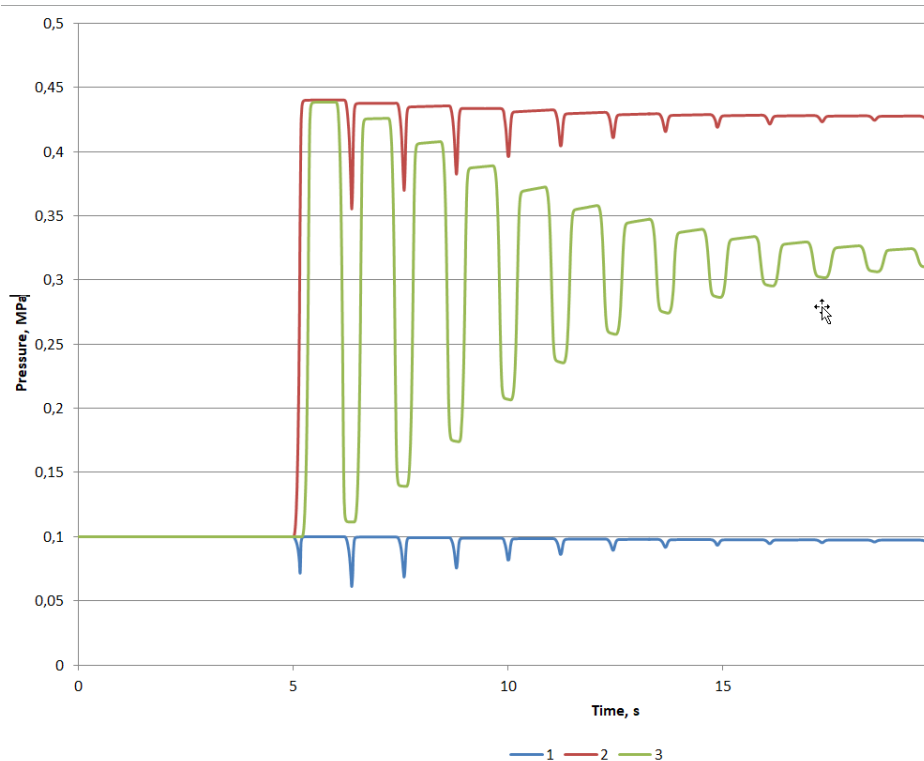
- If  $T_r \gg$  time of wave travel via piping ( $2L/c$ ), dynamic effects of pump transient operation are not significant
- Otherwise they should be analyzed!

# Example – pump shut down

- Discharge piping length 600 m.  $T_r$  - 0.2 s and 2 s.
- Points: 1 – pump inlet, 2 – outlet, 3 – middle of discharge piping



# The same example – pump start-up



# Questions for further investigation

- More data for Suter curves are needed!
- Other parameters (besides  $N_s$ ) for pump description
- How to deal with high viscosity fluid (when flow is not quadratic or even laminar)? Could HI viscosity corrections be used?
- How to deal with pump transient flow for settling slurries?
- How to deal with cavitation in the pump in transient operation?

**THANK YOU FOR YOU ATTENTION!**  
**Please visit PASS booth!**